## Descincontionio

## A CURE FOR INTRA-PAIR SKEW IN HIGH SPEED DIFFERENTIAL SIGNALS <br> E. XILINX <br> LL PROGRAMMABLEw

## Speaker

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## Effects of Intra-pair Skew

- Mode Conversion (increased Common Mode)
- Increased generation of EMI
- Increased susceptibility to EMI
- Less energy in differential signal reaching RX


## Causes of Intra-pair Skew

- Component and PCB layout asymmetries
- Manufacturing variability

Top Width:

- Top width less than foot -(0-0.5mils typical).
-Reduced with over etching
-Dependent on Cu oz and etch
factor.

0.5 mils along trace length.


Depression: - Close to full width - reduced height. - Unacceptable per IPC - Difficult to catch with AOI More common than admitted

- PCB Laminate Weave
- Rejectable if foot of trace is
reduced by $+/-20 \%$.
- Many shops will ship if reductions
<50\%

No Common Mode $\rightarrow$ No Skew

Zero common mode
$\rightarrow \operatorname{Vpos}(\mathrm{t})+\operatorname{Vneg}(\mathrm{t})=0$
$\rightarrow \operatorname{Vpos}(\mathrm{t})=-\operatorname{Vneg}(\mathrm{t})$
$\rightarrow$ when Vpos $=0$, Vneg $=0$ as well
$\rightarrow$ Zero skew

## Common Mode Block: Ground Plane Cuts



- Cuts in ground planes above and below strip line pair
- W \& Gap 2 to 3 times dielectric thickness
- L sets block center frequency (~Nyquist)
- $\mathrm{L}_{1,2} \sim \lambda / 4=[300 \mathrm{~mm} / \mathrm{ns}] /\left[4 * \operatorname{sqrt}\left(\varepsilon_{\mathrm{r}}\right)^{*} \mathrm{f}_{\text {Nyquist }}\right] \quad\left(\sim 150 \mathrm{mils} @ \mathrm{f}_{\text {Nyquist }}=10 \mathrm{GHz}\right)$
- Stagger $L_{1,2}$ for wider stop band (e.g., $L_{1}=130$ mils \& $L_{2}=170$ mils)
- This was developed heuristically - no pretense of optimality


## Common Mode Block: Alternatives

## An alternative, somewhat more complex design

[Yangyang Pang, Zhenghe Feng,
"A compact common-mode filter for GHz differential signals using defected ground structure and shorted microstrip stubs,"
2012 International Conference on Microwave and Millimeter Wave Technology (ICMMT),
Volume: 4, Publication Year: 2012 , Page(s): 1-4]

(a)

(b)

## Single-ended Cross-coupling



no GND Cutout
with GND Cutout

## Differential Pulse Response

- Coupling...
... delays effect of faster path

... accelerates effect of slower path
... minimizes common mode pulse response
... has negligible effect on differential pulse response

$1 \rightarrow 2 \& 3 \rightarrow 4$
$1 \rightarrow 4 \& 3 \rightarrow 2$


## Effect of GND Cutouts on Skew

16.7 Gb/s Pulse Response thru 6 inches of Megtron 6 strip line


## Differential Pulse Response vs. Skew

- Differential pulse responses with \& without CM filter nearly identical
- Low level ripple in pulse response with CM filter
- ...but smaller than a minor reflection in response without CM filter


## GND Cutout Geometries

## Common Mode Suppression:

Common Mode Insertion Loss / Differential Insertion Loss
$=$
SCC21 (dB) - SDD21 (dB)


## Common Mode Suppression



Common Mode Suppression




## Isn't this a Slot Antenna?

- Differential pairs on opposite sides of GND cutout
- Some energy ankathru-from_noir to pair, although most unbalanced energy is reflected back to transmitter
- Probably best to avoid using this technique with:
- parallel traces on adjacent planes
- cutouts in external GND planes
- microstrip traces



## Where Does the Power Go?

- Transmitted common mode power + power reflected back to transmitter by CM filter almost equal to transmitted power without CM filter



## Take Aways

- Skew is a growing problem at higher data rates
- Minimizing common mode also minimizes skew
- "Defected ground planes" can be effective common mode band reject filters
- Be careful not to make accidental antennas $\dot{\theta}^{\circ}$


## THANK YOU

## E. XILINX <br> ALL PROGRAMMABLE

